

Building Energy Efficiency Program

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TITLE

**Analysis of PFM02 window Using Computer Modeling According
to NFRC 500**

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PFM02

PFm02, which consists of a double-glazed window, has been modeled.

Thermo physical properties of different frame material are given in Table 1 and schematic representation of the material locations for a sill section is shown in Fig. 1. The detailed cross sections of the window system (case 3) are shown in Fig. 2.

Following 4 cases have been considered:

- Case 1: Without foam and no radiation enclosure
- Case 2: Without foam and with radiation enclosure
- Case 3: With foam and no radiation enclosure
- Case 4: With foam and with radiation enclosure

Table 1: Material Thermo physical Properties

Material	k (W/m-K)	ε
Aluminum Alloys	160.0	0.2
Polystyrene-Expanded (EPS)	0.035	0.9
Pine or Douglas Fir	0.14	0.9
Polyfoam tape	0.24	0.9
Silicone tape	0.36	0.9
Silica Gel (Desiccant)	0.03	0.9
Butyl Rubber	0.24	0.9
Urethane Sealant	0.31	0.9
Clear Glass	0.90	0.84

Window 4.1 has been used to create the glazing unit. The glazing unit is a 2 layered unit with CIG clear glass (ID 2003 in W4.1 glass library) as the outer layer and CIG SUN145 (ID 2018 in W4.1 glass library) as the inner layer . The filled gas is air, 0.65 inches for the gap. The detailed reports from Window4.1 are given in Appendix.

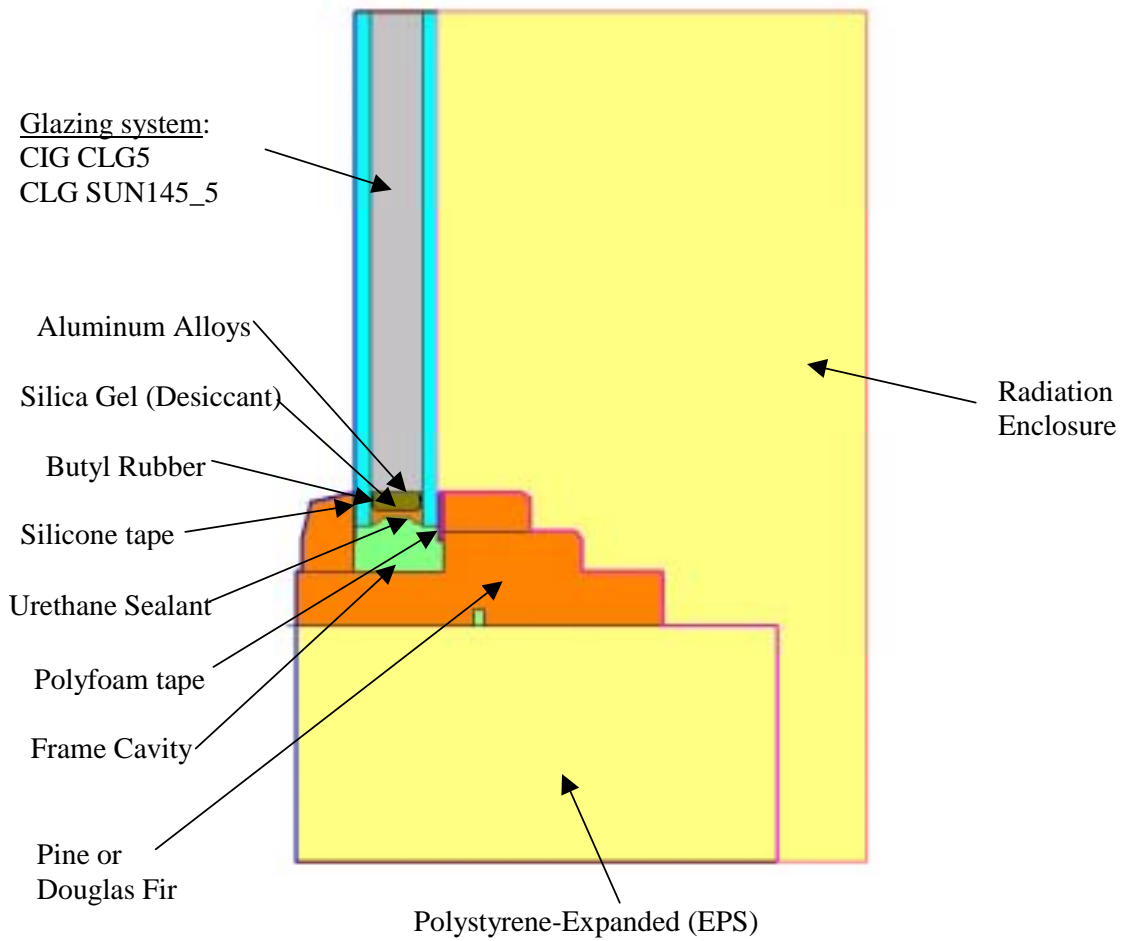


Fig. 1: Schematic representations of frame materials in a sill cross-section of frame (case 4)

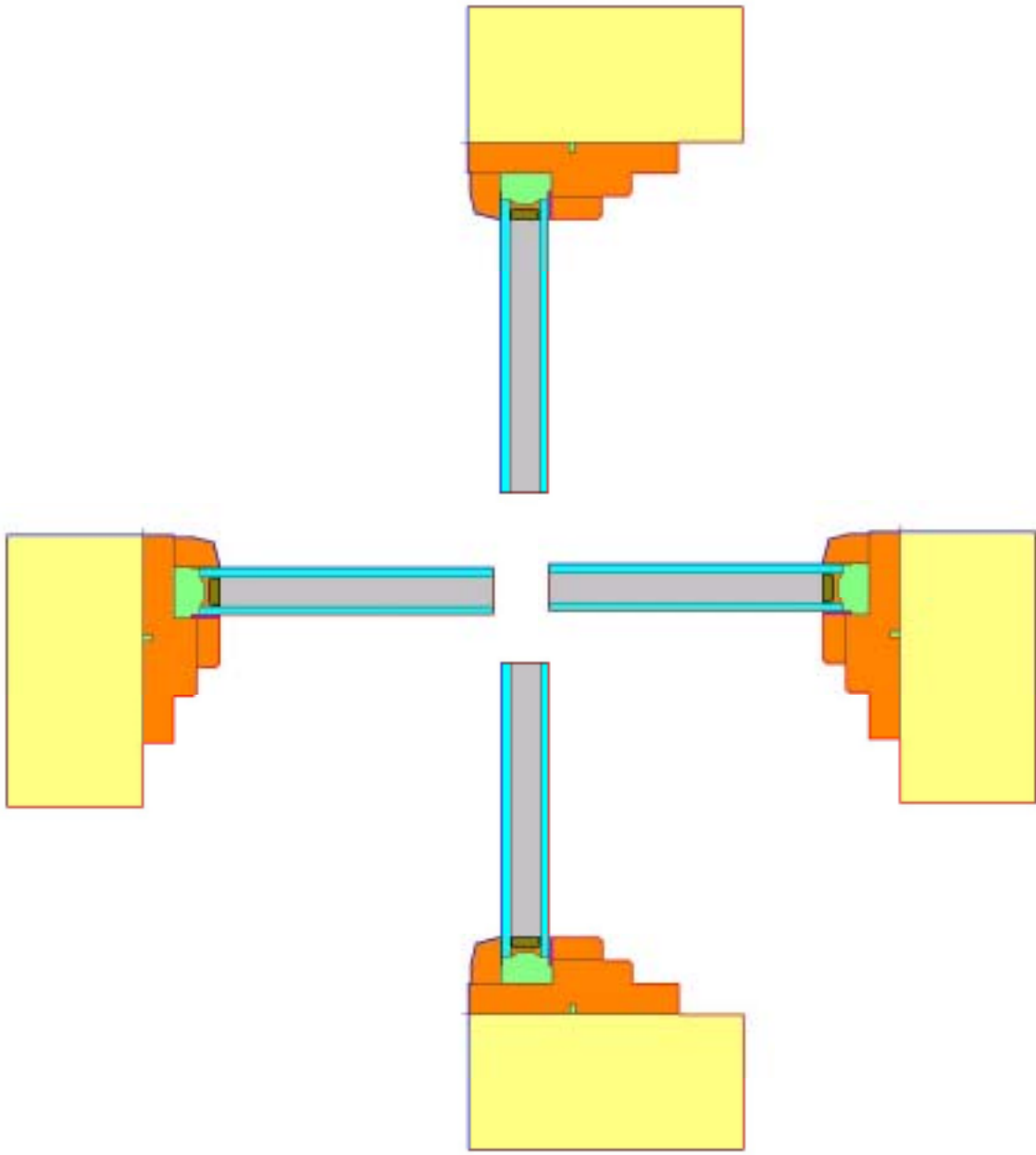


Fig. 2: Head, Jambs and sill cross sections of the window assembly (case3)

The isotherms for different cross sections of the window assembly (case 3) are shown in Fig. 3. Similar isotherms have been obtained for other cases. Calculations for case 1 and case 3 which are without radiation enclosure have been performed using the boundary conditions given in Table 2, while the other two cases using the boundary conditions given in Table 5.

Table 2: Boundary Conditions for Indoor and Outdoor Side of Window System case 1 , 3

<i>Boundary Conditions</i>		<i>Environmental Temperature (F)</i>	<i>Overall h</i>
			<i>(Btu/h-ft²-F)</i>
Outdoor Side	Edge-of-glass	0	5.112
	Frame		5.112
Indoor Side	Edge-of-glass	70	1.355
	Frame		1.340

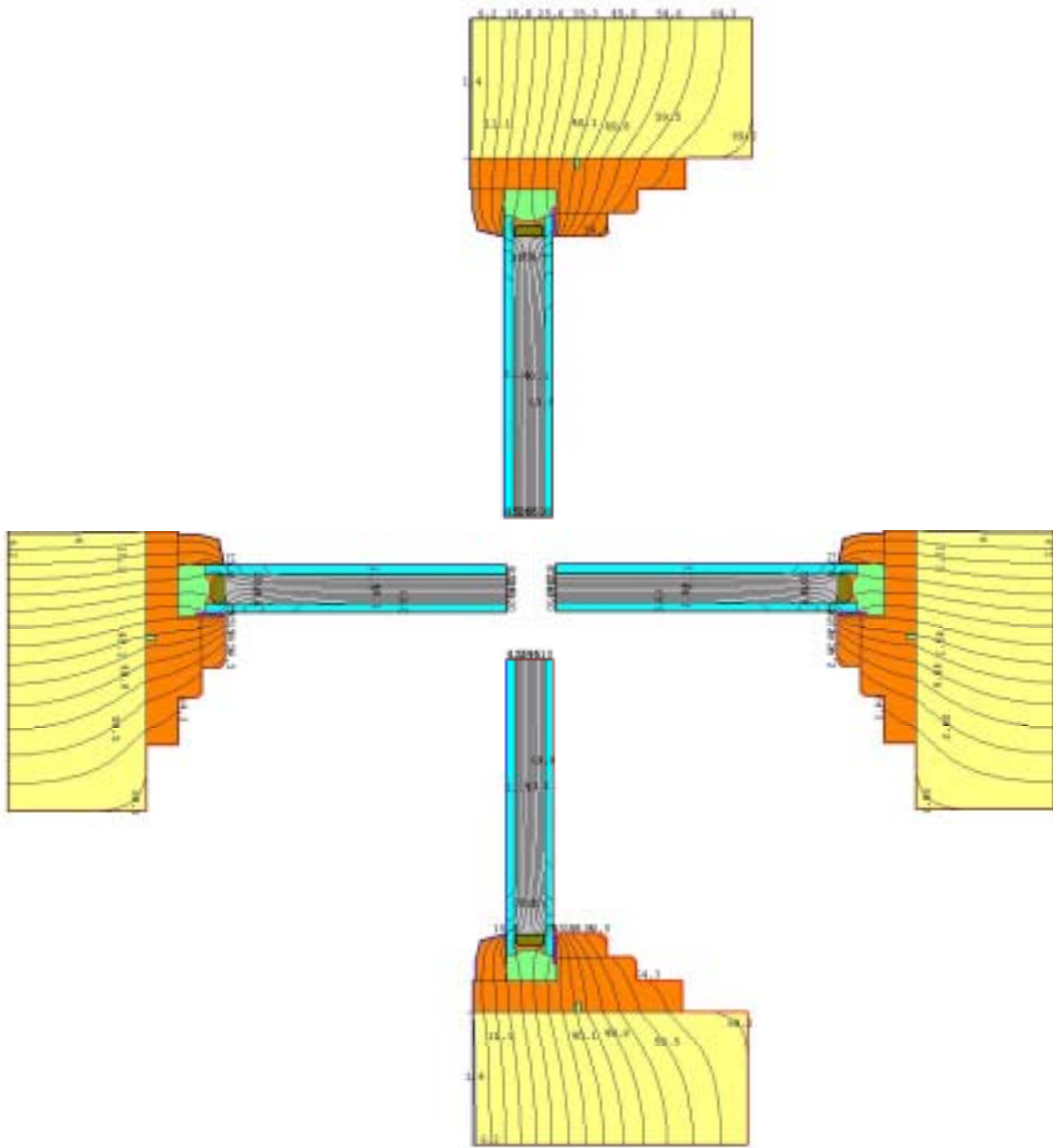


Fig. 3: Isotherms for head, jambs and sill Cross sections of the window system (case 3)

The frame and edge cross-sections U-factors and overall U-factors are given in Tables 3-6 respectively for all cases.

Table 3: Frame, Edge and Overall U-factors for Case 1 Window

<i>Cross Section</i>	<i>Name of THERM data file</i>	<i>Project Y of frame(inches)</i>	<i>U-factor of frame(Btu/h-ft²-F)</i>	<i>U-factor of edge-of-glass(Btu/h-ft²-F)</i>
Head	Pfm02_h_nRnf.thm	1.688	0.428	0.447
Sill	Pfm02_s_nRnf.thm	1.688	0.429	0.448
Jamb L	Pfm02_j_nRnf.thm	1.688	0.429	0.448
Jamb R	Pfm02_j_nRnf.thm	1.688	0.429	0.448
		<i>U-Factor (Btu/h-ft²-F)</i>	<i>SHGC</i>	<i>VT</i>
Center of glass		0.320	0.33	0.44
Window assembly		0.380	0.28	0.34

Table 4: Frame, Edge and Overall U-factors for Case 2 Window

<i>Cross Section</i>	<i>Name of THERM data file</i>	<i>Project Y of frame(inches)</i>	<i>U-factor of frame(Btu/h-ft²-F)</i>	<i>U-factor of edge-of-glass(Btu/h-ft²-F)</i>
Head	Pfm02_h_rnf.thm	1.688	0.441	0.436
Sill	Pfm02_s_rnf.thm	1.688	0.498	0.448
Jamb L	Pfm02_j_rnf.thm	1.688	0.498	0.448
Jamb R	Pfm02j_rnf.thm	1.688	0.498	0.448
		<i>U-Factor (Btu/h-ft²-F)</i>	<i>SHGC</i>	<i>VT</i>
Center of glass		0.320	0.33	0.44
Window assembly		0.392	0.28	0.34

Table 4: Frame, Edge and Overall U-factors for Case 3 Window

<i>Cross Section</i>	<i>Name of THERM data file</i>	<i>Project Y of frame(inches)</i>	<i>U-factor of frame(Btu/h-ft²-F)</i>	<i>U-factor of edge-of-glass(Btu/h-ft²-F)</i>
Head	Pfm02h_rnf.thm	1.688	0.461	0.450
Sill	Pfm02s_rnf.thm	1.688	0.465	0.452
Jamb L	Pfm02j_rnf.thm	1.688	0.465	0.452
Jamb R	Pfm02j_rnf.thm	1.688	0.465	0.452
		<i>U-Factor (Btu/h-ft²-F)</i>	<i>SHGC</i>	<i>VT</i>
Center of glass		0.320	0.33	0.44
Window assembly		0.389	0.28	0.34

Table 5: Frame, Edge and Overall U-factors for Case 4 Window

<i>Cross Section</i>	<i>Name of THERM data file</i>	<i>Project Y of frame(inches)</i>	<i>U-factor of frame(Btu/h-ft²-F)</i>	<i>U-factor of edge-of-glass(Btu/h-ft²-F)</i>
Head	Pfm02_h_rf.thm	1.688	0.424	0.429
Sill	Pfm02_j_rf.thm	1.688	0.428	0.430
Jamb L	Pfm02_j_rf.thm	1.688	0.428	0.431
Jamb R	Pfm02_j_rf.thm	1.688	0.428	0.431
		<i>U-Factor (Btu/h-ft²-F)</i>	<i>SHGC</i>	<i>VT</i>
Center of glass		0.320	0.33	0.44
Window assembly		0.375	0.28	0.34

Condensation Index:

Condensation Index (CI) has been calculated for case 4 with the boundary are shown in Fig. 4.

Table 5: Boundary Conditions for Indoor and Outdoor Side of Window System case 2, 4 and CI model for case 4

Boundary Conditions		Environmental Temperature (F)	h_c	Overall h	ε
			(Btu/h-ft ² -F)		
Outdoor Side	Glazing	0	N/A	5.112	0.84
	Frame		N/A	5.112	0.90
Indoor Side	Glazing	70	0.543	N/A	0.84
	Frame		0.444	N/A	0.90

Fig. 4 shows the schematic representation of head, jambs and sill cross sections (case 4). The jamb sections are modeled without radiation enclosure. The radiation enclosure has been used for the detailed radiation heat transfer calculations. Besides the method outlined in NFRC 500, CI calculations have been performed by the following three different methods:

Method 1 doesn't take area weighting for CI_g .

Method 2 takes area weighting of edge-of-glass area and center of glass area separately i.e. eqn (2) of NFRC 500 is divided into the following two parts:

$$CI_{cg} = \left\{ 1 - (SS_{cog})^{1/3} \right\} * 100$$

$$CI_{eog} = \left\{ 1 - \left(\frac{\sum_k SS_{eog_k} * A_{eog_k}}{A_{eog}} \right)^{1/3} \right\} * 100$$

CI_g is the minimum of the two, i.e. $CI_g = \text{Min} (CI_{cg}, CI_{eog})$

Method 3 is to take the CI value as the minimum value of CI_f and average of CI_{cog} and CI_{eog} , which are calculated using equations of Method 2.

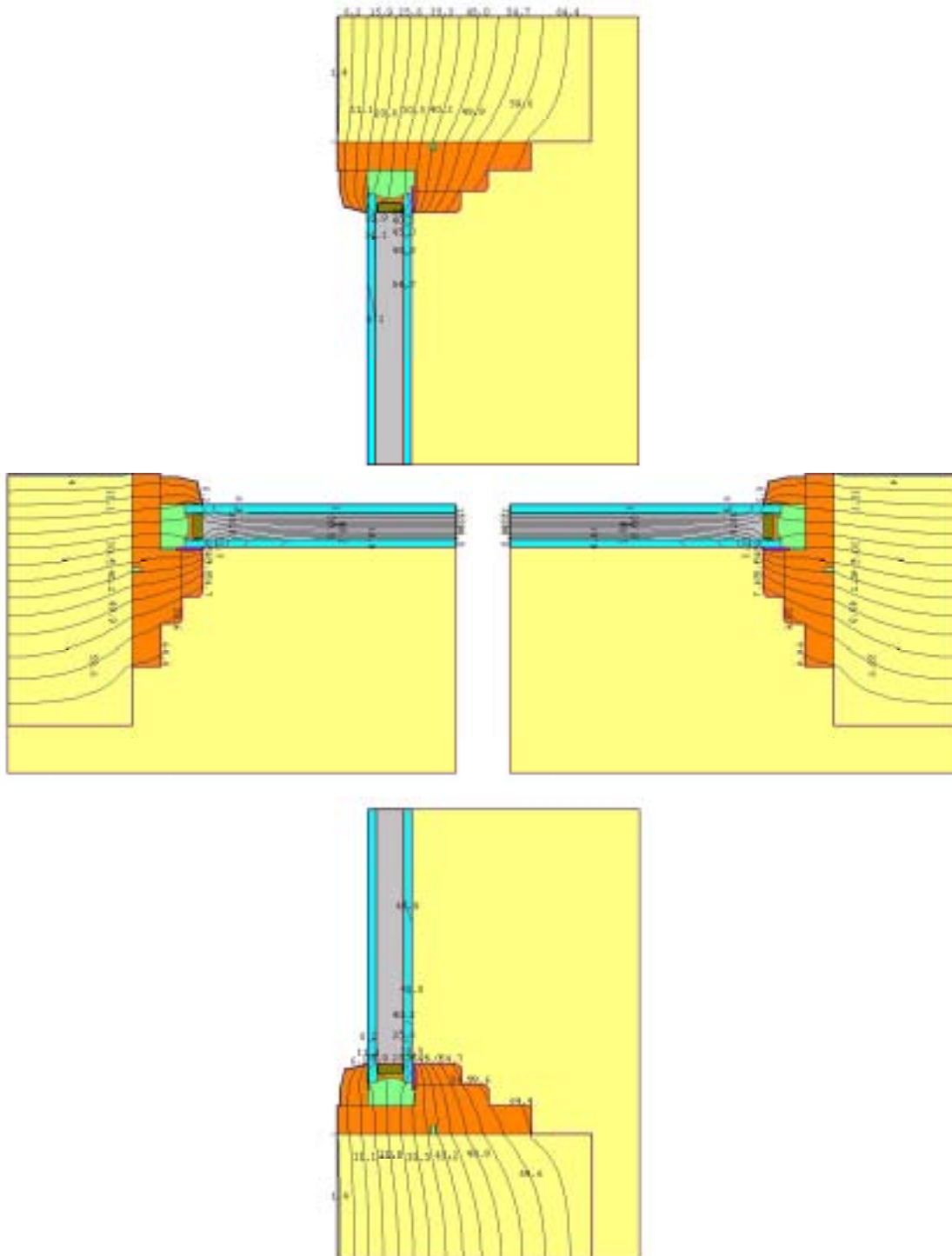


Table 6 shows the results calculated by using different methods.

Table 6: CI of windows using three different methods

	<i>Method 1</i>	<i>Method 2</i>	<i>Method 3</i>	<i>Current NFRC 500</i>
CI_f	68.30	68.30	68.30	68.30
CI_{cog}	-	66.07	-	-
CI_{eog}	-	48.95	-	-
CI_g	51.49	-	57.51	58.22
CI	51.49	48.95	57.51	58.22

Fig. 5 shows the temperature variation in the window assembly for both cases. The middle point in the graph corresponds to the center of glass temperature. Distance at X-axis corresponds to the bottom of sill section to the top of the head section.

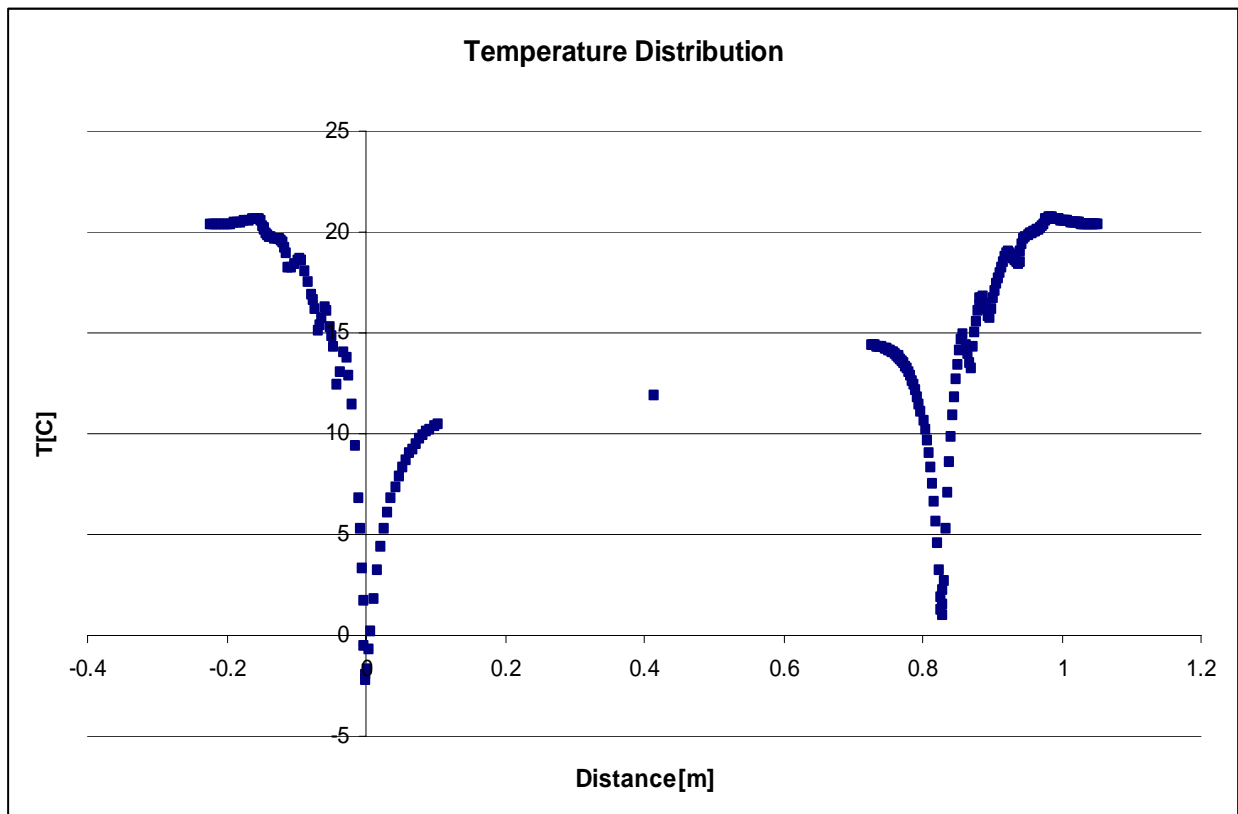


Figure 5. Temperature variation in the window assembly

Gas Data

ID	Name	Cond Btu/ h-ft- F	dCond Btu/h- ft-F2 x e-5	Visc lb-s/ ft2 x e-5	dVisc lb-s/ ft2-F x e-8	Dens lb/ft3	dDens lb/ft3- F	Pran	dPran
1	Air	.0139	2.4395	0.0361	0.1161	0.0805	-0.0002	.7200	.00100

Environmental Conditions: 1 NFRC/ASHRAE

	Tout (F)	Tin (F)	WndSpd (mph)	Wnd Dir	Solar (Btu/h-ft2)	Tsky	Esky (F)
Uvalue	0.0	70.0	15.00	Windward	0.0	0.0	1.00
Solar	89.0	75.0	7.50	Windward	248.2	89.0	1.00

Frame Library Data

ID	Name	Source	U-value		Edge	GlzSys	GlzSys	Width	Abs
			Frame	Edge	Corr	Width	Uc	(PFD)	
			Btu/h- ft2-F	Btu/h- ft2-F		in	Btu/h- ft2-F	in	
17	2_JAMB.T2W	FRAME Sill	0.43	0.43	N/A	1.0240	0.320	1.688	0.50
16	2_HEAD.T2W	FRAME Sill	0.42	0.43	N/A	1.0240	0.320	1.688	0.50
18	2_SILL.T2W	FRAME Sill	0.43	0.43	N/A	1.0240	0.320	1.688	0.50

Divider Library Data

ID	Name	Source	U-value		Edge	GlzSys	GlzSys	Width	Abs
			Div	Edge	Corr	Width	Uc	(PFD)	
			Btu/h- ft2-F	Btu/h- ft2-F		in	Btu/h- ft2-F	in	

No Dividers for this Glazing System

Angle 0 10 20 30 40 50 60 70 80 90 Hemis

Vtc : 0.443
 Rf : 0.153
 Rb : 0.137

Tsol : 0.267
 Rf : 0.226
 Rb : 0.248

Abs 1: 0.467
 Abs 2: 0.040
 Abs 3:
 Abs 4:
 Abs 5:
 Abs 6:
 SHGCc: 0.334

SCc: 0.39 Color Properties DomWL Purity L* a* b*
 Tdw: N/A Transmittance um %
 Tuv: N/A Reflectance um %

Temperature Distribution (degrees F) for '2 PFM02'

Env. Conditions:		1 NFRC/ASHRAE	U-value	Condensation RH	Solar
	Outside Air		0.0		89.0
	Outer Surface		4.5	N/A	115.3
Layer 1	Center		4.8		116.9
	Inner Surface		5.1		116.7
	Outer Surface		52.8		90.5
Layer 2	Center		53.1		90.4
	Inner Surface		53.5	55.7%	90.0
	Inside Air		70.0		75.0